

Features

- 3A output Current
- Automatic Pulse Skipping Mode at Light Load
- Integrated $142m\Omega/103m\Omega$ DMOS Switches
- 4.5V to 30V Input Operating Range
- Output Adjustable from 0.92V to 20V
- Up to 94% Efficiency
- 3uA Shutdown Current
- Fixed 340KHz Frequency
- Programmable Soft-Start
- Thermal Shutdown and Overcurrent Protection
- Input Supply Overvoltage and Undervoltage Lockout
- 220ns Minimum On Time
- RoHS Compliant and 100% Lead(pb)-Free Halogen-Free

Applications

- Distributed Power Systems
- Networking Systems
- PC Monitors
- Portable Electronics

General Description

The HCR3234 is a synchronous current mode buck regulator capable of driving 3A continuous load current with excellent line and load regulation.

The HCR3234 can operate with an input range 4.5V to 30V and the output can be externally set from 0.92V to 20V with a resistor driver.

Fault condition protection includes cycle-by-cycle current limiting and thermal shutdown, in shutdown mode the regulator draws 3uA of supply current.

Programmable soft-start minimizes the inrush supply current and the output overshoot at initial startup. Automatic pulse skipping mode operation increase efficiency at light loads.

The HCR3234 require a minimum number of external components. It is available in SOP-8(EP) Pacakge.



Figure 1. Package Type of HCR3234



Pin Configuration

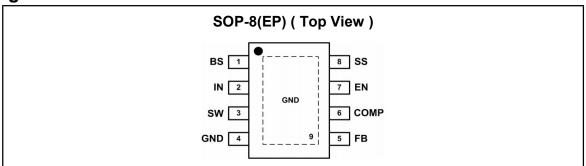


Figure 2. Pin Configuration of HCR3234 (Top View)

Pin Function Table

Pin Number	Pin Name	Function
1	BS	High-side Gate Drive Boost Input. BS supplies the drive for the high-side N-channel DMOS switch. Connect a 0.01uF or greater capacitor from SW to BS to power the high side switch.
2	IN	Input Supply Pin. IN supplies the power to the IC, as well as the step-down converter switches. Drive IN with a 4.5V to 30V power source. Bypass IN to GND with a suitably large capacitor to minimize input ripple to the IC.
3	sw	Power Switching Output. Connect the output LC filter from SW to the output load.
4 9(Exposed Pad)	GND	Ground. GND Pin should be connected to the exposed thermal pad for proper operation. This power thermal pad should be connected to PCB ground plane using multiple vias for good thermal performance.
5	FB	Output Feedback Input. FB senses the output voltage and regulates it. Drive FB with a resistive voltage divider connected to it from the output voltage. The feedback threshold is 0.92V.
6	COMP	Loop compensation Input. Connect a series RC network from COMP to GND to compensate the regulation control loop.
7	EN	Enable Input. EN is a logic input that controls the regulator on or off. Drive EN high to turn on the regulator, low to turn it off. Don't leave EN pin floating. Directly connect EN to IN (or through a resistance) for automatic startup.
8	SS	Soft-start Control Input. Connect an external capacitor to program the soft-start. If unused, leave it open, which means internal soft-start function.

Ordering Information



Ordering Code

Part Number	Marking ID ²	Temperature Range	Package	Quantity per Reel
HCR3234/ADJM8ETR	HCR3234XXX	-40'C to +85'C	SOP-8(EP)	4000pcs/TR

Note2: the HCR3234 is type and "XXX" is date code.



Absolute Maximum Ratings Note 1

Symbol	Value	Unit
Vin	-0.3 to +34	V
VEN	-0.3 to +34	V
Vsw	-1 to VIN +0.3	V
VBS	VSW-0.3 to VSW +6	V
-	-0.3 to +6	V
Vоит	0.92 to 20	v
PD	2.083	w
Reja	60	'C/W
Rejc	20	'C/W
Тѕтс	-65 to 150	'C
TJ	-40 to 150	'C
TLEAD	260	'C
	VIN VEN VSW VBS - VOUT PD Reja Rejc Tstg	Vin -0.3 to +34 VEN -0.3 to +34 VSW -1 to VIN +0.3 VBS VSW-0.3 to VSW +6 - 0.3 to +6 VOUT 0.92 to 20 PD 2.083 ReJA 60 ReJC 20 TSTG -65 to 150 TJ -40 to 150

Recommend Operating Conditions note2

Input Voltage	VIN	4.5 to 30	V
Ambient Operting Temp	TA	-40 to +85	ō

Note 1: Stresses beyond those listed under "Absolute maximum Ratings" may damage the device.

2: The device is not guaranteed to function outside the recommended operating conditions.



Electrical Characteristics

The specifications which apply over the full operating temperature range, otherwise specification

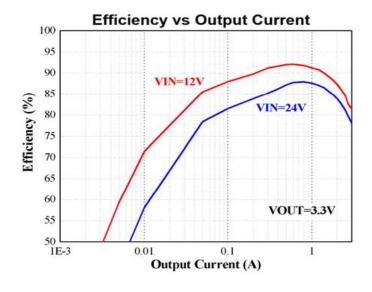
are VIN=12V, (Ta=25'C; unless otherwise specified)

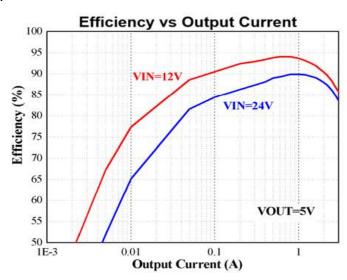
are VIN=12V, (Ta=25°C; unless otherwi	se speciti	ea)		1		1
Parameter	Symbol	Test Condition	Min	Туре	Max	Unit
Input Operation Voltage	Vin		4.5	-	30	V
Shutdown Supply Current	Іѕтву	Ven=0V	•	3	5	uA
Quiescent Supply Current	lq	V _{FB} =1V		1	1.4	mA
Feedback Voltage	VFB	4.5V <= VIN <= 30V	0.902	0.92	0.938	V
Error Amplifier Voltage Gain			-	800	-	V/V
Error Amplifier Transconductance		Δlc=+/-10uA	-	650	-	u A /V
High-side Switch On-Resistance	RHS		-	142	-	mΩ
Low-side Switch On-Resistance	RLS		-	103	-	mΩ
High-side Switch Leakage Current	lleakage	VEN=0, VSW=0V	-	-	5	uA
Upper Switch Current Limit	ILH	Minimum Duty Cycle	3.8	5.5	-	Α
Lower Switch Current Limit	lLO	From Drain to source	-	0	-	Α
COMP to Current Sense Transconductance	Iccs		-	4.5	-	A/V
Oscillator Frequency	Fosc		300	340	380	KHz
Short Circuit Oscillator Frequency	Fsнт	VFB=0V	-	110	-	KHz
Maximum Duty Cycle	DMAX	VFB=0.7V	-	96	-	%
Minimum On Time	Ton		-	220	-	ns
EN Langué Valéa de	M	EN High Threshold	2.0	-	-	
EN Input Voltage	VEN	EN Low Threshold	-	-	0.4	\
Input Under Voltage Lockout Threshold	VLK	VIN Rising	3.8	4.1	4.4	v
Soft-start Charge Current	İstart	Vss=0V	-	6	-	uA
Thermal Shutdown	Tstdn		-	160	-	'C

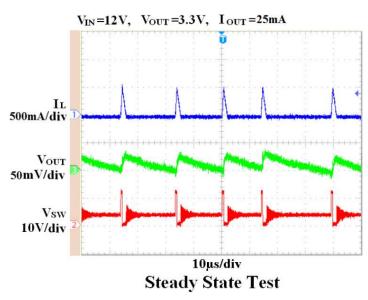


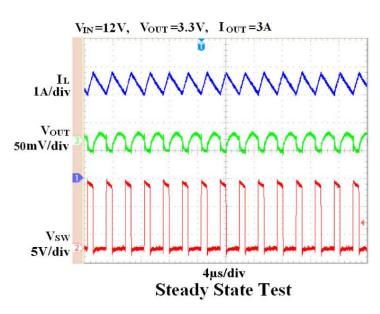
Typical Performance Characteristics

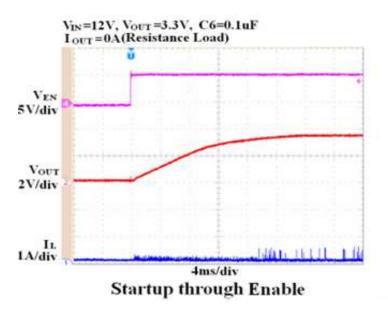
(See Figure 4, C1=10uF, C2=22uFX2, L=10uH, TA=+25'C)

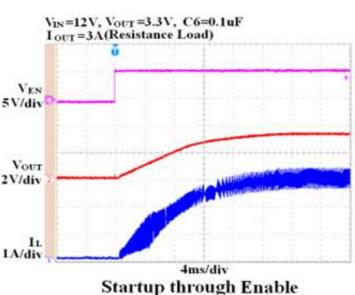








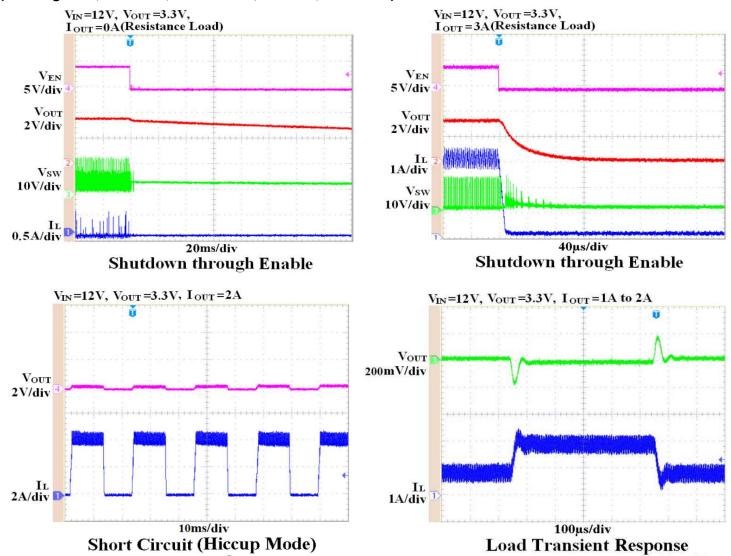






Typical Performance Characteristics (continued)

(See Figure 4, C1=10uF, C2=22uFX2, L=10uH, TA=+25'C)



Functional Block Diagram

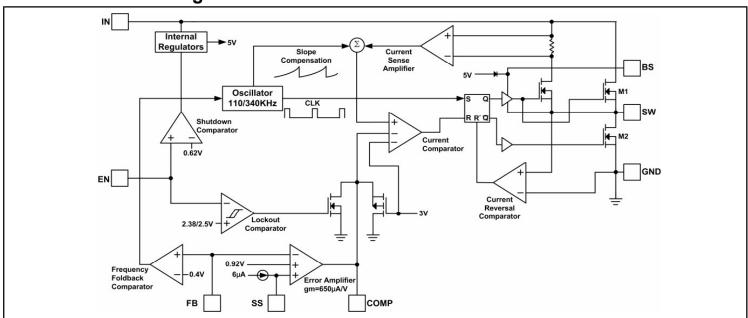


Figure 3. Functional Block Diagram of HCR3234



Typical Application Circuit

Input Voltage 12V to 3.3V or 5.0V / 3A Application Circuit

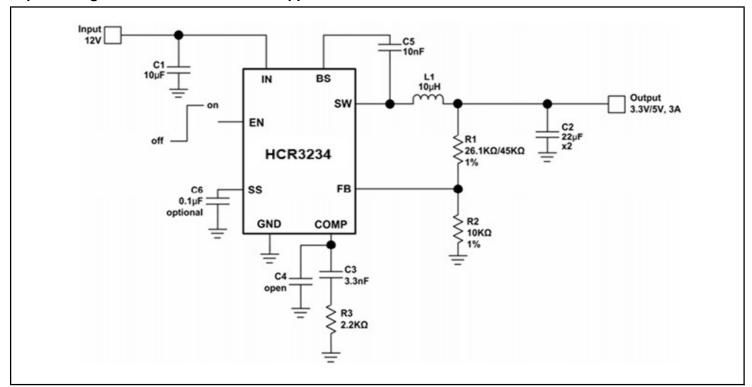


Figure 4. Adjustable Output Voltage of HCR3234

Input Voltage 30V to 3.3V or 5.0V / 3A Application Circuit

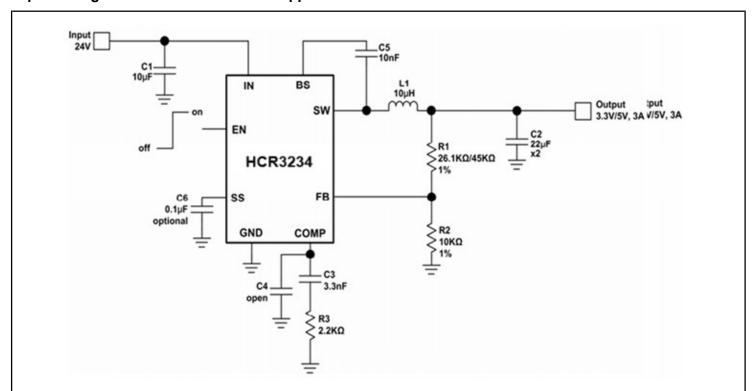


Figure 5. 30V to 3.3V or 5V Application Circuit of HCR3234



Function Description

The HCR3234 regulates input voltages from 4.5V to 30V down to an output voltage as low as 0.92V, and supplies up to 3A of load current.

The HCR3234 uses current-mode control to regulated the output voltage. The output voltage is measured at FB through a resistive voltage divider and amplified through the internal transconductance error amplifier.

The voltage at the COMP pin is compared to the switch current (measured internally) to control the output voltage.

The converter uses internal N-Channel MOSFET switch to step-down the input voltage to the regulated output voltage. Since the high side MOSFET requires a gate voltage greater than the input voltage, a boost

capacitor connected between SW and BS is needed to drive the high side gate. The boost capacitor is charged from the internal 5V rail when SW is low. At light loads, the inductor current may reach Zero or reverse on each pulse. The bottom DMOS is turned off by the current reversal comparator and the switch voltage will ring. This is discontinuous mode operation, and is normal behavior for the switching regulator. At light load, the HCR3234 will automatically skip pulses in pulse skipping mode operation to maintain output regulation and increase efficiency.

When the FB pin voltage exceeds 13% of the nominal regulation value of 0.92V, the over voltage comparator is tripped and forcing the high-side switch off.

Application Information

Setting the Output Voltage

The output voltage is set using a resistive voltage divider connected from the output voltage to FB. The voltage divider divides the output voltage down to the feedback voltage by the ratio:

$$V_{FB} = V_{OUT} \frac{R2}{R1 + R2}$$

Thus the output voltage is:

$$V_{OUT} = 0.92 * \frac{R1 + R2}{R2}$$

R2 can be as high as $100K\Omega$, but a typical value is $10K\Omega$ Using the typical value for R2, R1 is determined by:

$$R1 = 10.81 * (V_{OUT} - 0.92)$$
 (k Ω)

For example, for a 3.3V output voltage, R2 is $10K\Omega$ and R1 is $26.1K\Omega$.

Inductor

The inductor is required to supply constant current to the load while being driven by the switched input voltage. A larger value inductor will result in less ripple current that will in turn result in lower output ripple voltage. However, the larger value inductor will have a large physical size, higher series resistance, and/or lower saturation current. A good rule for determining inductance is to allow the peak-to-peak ripple current to be approximatelly 30% of the maximum switch current limit. Also, make sure that the peak inductor current is below the maximum switch current

Inductor (Con.)

limit. The inductance value can be calculated by:

$$L = \frac{V_{OUT}}{f_{S} * \Delta I_{L}} * \left(1 - \frac{V_{OUT}}{V_{IN}}\right)$$

Where VOUT is the output voltage, VIN is the input voltage, f_S is the switching frequency, and ΔIL is the peak-to-peak inductor ripple current.

Choose an inductor peak current, calculated by:

$$I_{LP} = I_{LOAD} + \frac{V_{OUT}}{2 * f_S * L} * \left(1 - \frac{V_{OUT}}{V_{IN}}\right)$$

Where ILOAD is the load current.

The choice of which style inductor to use mainly depends on the price vs.size requirements and any EMI constraints.

Optional Schottky Diode

During the transition between the high-side switch and low-side switch, the body diode of the low-side power MOSFET conducts the inductor current. The forward voltage of this body diode may be high and cause efficiency loss. An optional small 1A Schottky diode B130 in parallel with low-side switch is recommended to improve overall efficiency when input voltage is higher.

Input Capacitor

The input current to the step-down converter is discontinuous, therefore a capacitor is required to supply the AC current while maintaining the DC input voltage. Use low ESR capacitors for the best



Application Information(Con,)

performance. Ceramic capacitors are preferred, but tantalum or low-ESR electrolytic capacitors will also suffice. Choose X5R or X7R dielectrics when using ceramic capacitors.

Since the input capacitor (C1) absorbs the input switching current, it requires an adequate ripple current rating. The RMS current in the input capacitor can be estimated by:

$$I_{C1} = I_{LOAD} * \sqrt{\frac{V_{OUT}}{V_{IN}}} * \left(1 - \frac{V_{OUT}}{V_{IN}}\right)$$

The worst-case condition occurs at V_{IN}=2V_{OUT}, where

Ic1=ILOAD/2. For simplification, use an input capacitor with a RMS current rating greater than half of the maximum load current.

The input capacitor can be electrolytic, tantalum or ceramic, When using electrolytic or tantalum capacitors, a small, high quality ceramic capacitor, i.e.0.1uF, should be placed as close to the IC as possible. When suing ceramic capacitors, make sure that they have enough capacitance to provide sufficient charge to prevent excessive voltage ripple at input. The input voltage ripple for low ESR capacitors can be estimated by:

$$\Delta V_{IN} = \frac{I_{LOAD}}{Cl * f_{S}} * \frac{V_{OUT}}{V_{IN}} * \left(1 - \frac{V_{OUT}}{V_{IN}}\right)$$

Where C1 is the input capacitance value. For simplification, choose the input capacitor whose RMS current rating greater than half of the maximum load current.

Output Capacitor

The output capacitor(C2) is required to maintain the DC output voltage. Ceramic, tantalum, or low ESR electrolytic capacitors are recommended. Low ESR capacitors are preferred to keep the output voltage ripple low. The output voltage ripple can be estimated

$$\Delta V_{\text{OUT}} = \frac{V_{\text{OUT}}}{f_{\text{S}} * L} * \left(1 - \frac{V_{\text{OUT}}}{V_{\text{IN}}} \right)$$
$$* \left(R_{\text{ESR}} + \frac{1}{8 * f_{\text{S}} * C2} \right)$$

Where C2 is the output capacitance value and RESR is the equivalent series resistance (ESR) value of the output capacitor. when using ceramic capacitors, the impedance at the switching frequency is dominated by the capacitance which is the main cause for the output voltage ripple. for simplification, the output

Output Capacitor(Con.)

voltage ripple can be estimated by:

$$\Delta V_{OUT} = \frac{V_{OUT}}{8 * f_{S}^{2} * L * C2} * \left(1 - \frac{V_{OUT}}{V_{IN}}\right)$$

When using tantalum or electrolytic capacitors, the ESR dominates the impedance at the switching frequency. For simplification, the output ripple can be approximated to:

$$\Delta V_{OUT} = \frac{V_{OUT}}{f_{S} * L} * \left(1 - \frac{V_{OUT}}{V_{IN}}\right) * R_{ESR}$$

The characteristics of the output capacitor also affect the stability of the regulation system. The HCR3234 can be optimized for a wide range of capacitance and ESR values.

Compensation Components

The HCR3234 employs current mode control for easy compensation and fast transient response. The system stability and transient response are controlled through the COMP pin. COMP is the output of the internal transconductance error amplifier. A series capacitor resistor combination sets a pole-zero combination to govern the characteristics of the control system. The DC gain of the voltage feedback loop is given by:

$$A_{VDC} = R_{LOAD} *G_{CS} *A_{VEA} * \frac{V_{FB}}{V_{OUT}}$$

Where VFB is the feedback voltage (0.92V), AVEA is the error amplifier voltage gain, Gcs is the current sense transconductance and RLOAD is the load resistor value.

The system has two poles of importance. One is due to the compensation capacitor(C3) and the output resistor of the error amplifier, and the other is due to output capacitor and the load resistor.

These poles are located at:

$$f_{P1} = \frac{G_{EA}}{2\pi * C3 * A_{VEA}}$$
$$f_{P2} = \frac{1}{2\pi * C2 * R_{LOAD}}$$

Where GEA is the error amplifier transconductance. the system has one zero of importance, due to the compensation capacitor (C3) and the compensation resistor(R3). This zero is located at:

$$f_{Z1} = \frac{1}{2\pi * C3 * R3}$$

The system may have another zero of importance, if the output capacitor has a large capacitance and/or a



Application Information(Con,)

Compensation Components(con.)

high ESR value. The zero, due to the ESR and capacitance of the output capacitor, is located at:

$$f_{ESR} = \frac{1}{2\pi * C2 * R_{ESR}}$$

In this case, a third pole set by the compensation capacitor (C4) and the compensation resistor (R3) is used to compensate the effect of the ESR zero on the loop gain. This pole is located at:

$$f_{P3} = \frac{1}{2\pi * C4 * R3}$$

The goal of compensation design is to shape the converter transfer function to get a desired loop gain. the system crossover frequency where the feedback loop has the unity gain is important. Lower crossover frequencies result in slower line and load transient responses, while higher crossover frequencies could cause the system instability. A good standard is to set the crossover frequency below one-tenth of the switching frequency.

To optimize the compensation components, the following procedure can be used:

1.1 Choose the compensation resistor(R3) to set the desired crossover frequency.

Determine R3 by the following equation:

$$R3 = \frac{2\pi * C2 * f_{C}}{G_{EA} * G_{CS}} * \frac{V_{OUT}}{V_{FB}}$$

$$< \frac{2\pi * C2 * 0.1 * f_{S}}{G_{EA} * G_{CS}} * \frac{V_{OUT}}{V_{FB}}$$

Where fc is the desired crossover frequency, which is typically below one tenth of the switching frequency.

1.2 Choose the compensation capacitor(C3) to achieve the desired phase margin. For applications with typical inductor values, setting the compensation zero (fz1) below one-forth of the crossover frequency provides sufficient phase margin. Determine C3 by the following equation:

$$C3 > \frac{4}{2\pi * R3 * f_C}$$

Where R3 is the compensation resistor.

1.3 Determine if the second compensation capacitor (C4) is required. It is required if the ESR zero of the output capacitor is located at less than half of the switching frequency, or the following relationshop is valid: $\frac{1}{2\pi*C2*R} < \frac{f_S}{2}$

If this is the case, then add the second compensation capacitor (C4) to set the pole fp3 at the location of the ESR zero. Determine C4 by the equation:

$$C4 = \frac{C2 * R}{R3}$$

To simplify design efforts using the HCR3234, the typical design for common application are listed in Table 1.

External Bootstrap Diode

It is recommended that an external bootstrap diode be added when the system has a 5V fixed input or the power supply generates a 5V output. This helps improve the efficiency of the regulator.

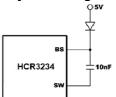


Figure 6. Add optional External Bootstrap

Diode to Enhance

This diode is also recommended for high duty cycle operation (When Vout/Vin >65%) and high output Voltage (Vout > 12V) applications.

Table 1. External Components for Typical Designs

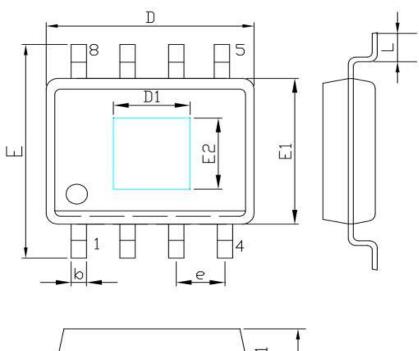
Vin(V)	Vout(V)	L1(uH)	C2 (uF)	R1(KΩ)	R2(KΩ)	R3(KΩ)	C3(nF)	C4(pF)
5	1.0	3.3	22*2	1.0	10	2.2	3.3	open
5	1.2	4.7	22*2	3.2	10	2.2	3.3	open
5	3.3	10.0	22*2	26.1	10	2.2	3.3	open
12	1.0	3.3	22*2	1.0	10	2.2	10.0	open
12	1.2	4.7	22*2	3.2	10	2.2	10.0	open
12	3.3	10.0	22*2	26.1	10	2.2	3.3	open
12	5.0	10.0	22*2	45.0	10	2.2	3.3	open
24	3.3	10.0	22*2	26.1	10	2.2	3.3	open
24	5.0	10.0	22*2	45.0	10	2.2	3.3	open

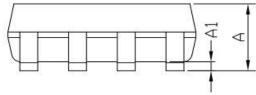


Mechanical Dimensions



Unit: mm(inch)



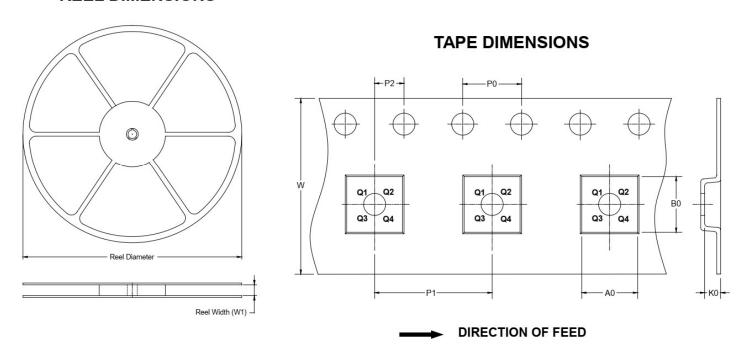


SYMBOLS	M	ILLIMETERS	3	INCHES		
SIMBOLS	MIN.	Normal	MAX.	MIN.	Normal	MAX.
A	1.35	-	1.75	0.053	-	0.069
A1	0.00	-	0.25	0.000	-	0.010
D	4.80	4.90	5.00	0.189	0.193	0.197
E1	3.70	3.90	4.00	0.146	0.154	0.157
D1	2.67	2.97	3.50	0.105	0.117	0.138
E2	1.78	2.18	2.60	0.070	0.086	0.102
Е	5.80	6.00	6.20	0.228	0.236	0.244
L	0.40	-	1.27	0.016	-	0.050
b	0.31	-	0.51	0.012	-	0.020
e		1.27 REF			0.050 REF	



TAPE AND REEL INFORMATION

REEL DIMENSIONS



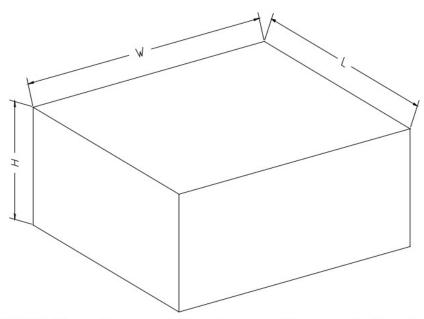
NOTE: The picture is only for reference. Please make the object as the standard.

KEY PARAMETER LIST OF TAPE AND REEL

Package Type	Reel	Reel Width W1	A0	В0	K0	P0	P1	P2	w	Pin1
i donago Typo	Diameter	(mm)	(mm)	(mm)	(mm)	(mm)	(mm)	(mm)	(mm)	Quadrant
SOP-8(EP)	13"	12.4	6.40	5.40	2.10	4.0	8.0	2.0	12.0	Q1



CARTON BOX DIMENSIONS



NOTE: The picture is only for reference. Please make the object as the standard.

KEY PARAMETER LIST OF CARTON BOX

Reel Type	Length (mm)	Width (mm)	Height (mm)	Pizza/Carton
13"	386	280	370	5